

CIVL3140 Introduction to Open Channel Hydraulics - TUTORIAL 2

1. Application of the Bernoulli principle

1.1. Considering a trapezoidal channel (1V:3H sideslopes, 1.5 m bottom width), calculate the critical depth d_c for $Q = 3 \text{ m}^3/\text{s}$ and $10 \text{ m}^3/\text{s}$.

Solution: see textbook pp. 44-46

1.2. Considering a smooth transition, the flow rate is $7.2 \text{ m}^3/\text{s}$. The channel upstream and downstream cross-sections are:

upstream : rectangular, $B = 5 \text{ m}$, $z_0 = 0.5 \text{ m}$

downstream : rectangular, $B = 3.9 \text{ m}$, $z_0 = 0.2 \text{ m}$

(a) if the upstream water depth equals 1.9 m, calculate the downstream water depth

(b) if the upstream water depth equals 0.8 m, calculate the downstream Froude number

Numerical solution : (a) $d_1 = 1.9 \text{ m} \Rightarrow d_2 = 2.19 \text{ m}$ (b) $d_1 = 0.8 \text{ m} \Rightarrow d_2 = 1.13 \text{ m}$

2. Application of the Momentum principle

2.1 Application of the continuity and momentum principles to a hydraulic jump

A hydraulic jump takes place in a rectangular channel (10-m wide). The total flow rate is 187,500 L/s and the upstream flow depth is 1.4 m. Compute and give the values (and units) of the following quantities : (a) upstream Froude number, (b) type of jump, (c) downstream flow depth, (d) downstream flow velocity, (e) total head loss, (f) hydraulic power dissipated in the jump, (g) If the dissipated power could be transformed into electricity, how many 100-W bulbs could be lighted ?

Numerical solution: $Fr_1 = 3.62$, $d_2 = 6.49 \text{ m}$ (d/s depth), $\Delta H = 3.63 \text{ m}$

2.2 At the end of a steep chute, a hydraulic jump is forced in the downstream stilling basin. The basin is a horizontal rectangular channel ($B = 22.5 \text{ m}$). The observed downstream flow depth is 2.1 m and the discharge is $46 \text{ m}^3/\text{s}$.

(2.2.1) Compute and give the values (and units) of the following quantities : (a) upstream Froude number, (b) type of jump, (c) hydraulic power dissipated in the jump.

(2.2.2) What basic principle(s) was(were) used to compute the upstream flow depth ?

(2.2.3) Describe (in words) the characteristics of this type of hydraulic jump

Solution : the flow conditions correspond to a steady hydraulic jump. See textbook pp. 60 & 412-417.

Numerical solution: $Fr_1 = 8.7$, $d_1 = 0.18 \text{ m}$, $\Delta H = 4.76 \text{ m}$

2.3 Considering the flow upstream of a sluice gate, the gate closes suddenly. The initial flow conditions were : $Q = 5.2 \text{ m}^3/\text{s}$, $d = 2 \text{ m}$, $B = 3 \text{ m}$. The new discharge is : $Q = 2.2 \text{ m}^3/\text{s}$. Compute the new flow depth and flow velocity. *The channel is smooth, rectangular, and horizontal.*

Solution: Upstream of the gate, the flow conditions associated with a reduction in discharge correspond to the formation of a positive surge.

Numerical solution: $V_{\text{srg}} = 3.97 \text{ m/s}$, $v_2 = 0.33 \text{ m/s}$, $d_2 = 2.25 \text{ m}$

2.4 A bore is a positive surge of tidal origin which may form with large tidal ranges in a converging channel forming a funnel shape. The front of the surge absorbs random disturbances on both sides and this makes the wave stable and self-perpetuating (HENDERSON 1966, CHANSON 1999). With appropriate boundary conditions, a tidal bore may travel long distances upstream: e.g., the tidal bore on the Pungue river (Mozambique) is still about 0.7 m high about 50

km upstream of the mouth and it may reach 80 km inland. Famous bores include the Hangzhou (or Hangchow) bore on the Qiantang river, the Amazon bore called *pororoca*, the tidal bore on the Seine river (*mascaret*) and the Hoogly (or Hooghly) bore on the Gange. Smaller tidal bores occur on the Severn river near Gloucester, England, on the Dordogne river, France, in the Bay of Fundy (at Petitcodiac and Truro), on the Styx and Daly rivers (Australia), and at Batang Lupar (Malaysia) (see Figure below).

A tidal bore affects shipping industries. For example, the *mascaret* of the Seine river had had a sinister reputation. More than 220 ships were lost between 1789 and 1840 in the Quilleboeuf-Villequier section (MALANDAIN 1988). The height of the *mascaret* bore could reach up to 7.3 m and the bore front travelled at a celerity of about 2 to 10 m/s. Even in modern times, the Hoogly and Hangzhou bores are hazards for small ships and boats. Tidal bores affect also estuarine eco-systems. The effect on sediment transport was studied at Petitcodiac and Shubenacadie rivers, on the Sée and Sélune rivers and on the Hangzhou bay. The impact on the ecology is acknowledged in the Amazon where piranhas eat matter in suspension after the passage of the bore, at Turnagain Arm where bald eagles fish behind the bore, in the Severn river (sturgeons in the past, elvers) and in the Bay of Fundy (striped bass spawning).

On the 27 Sept. 2000, the flow conditions of the tidal bore of the Dordogne river were : initial water depth = 1.5 m, initial flow velocity = +0.22 m/s, observed bore celerity : 4.8 m/s. Assuming a wide rectangular channel, calculate the flow velocity after the passage of the bore. (Use the downstream flow direction as positive axis.)

Tidal bore of the Dordogne river on 27 Sept. 2000, looking downstream at the arriving bore



Additional references

- CHANSON, H. (2001). "Flow Field in a Tidal Bore : a Physical Model." *Proc. 29th IAHR Congress*, Beijing, China, Theme E, Tsinghua University Press, Beijing, G. LI Ed., pp. 365-373 (ISBN 7-302-04676-X/TV). (CD-ROM, Tsinghua University Press, ISBN 7-900637-10-9.)
- CHANSON, H. (2005). "Tidal Bore Processes in the Baie du Mont Saint Michel (France): Field Observations and Discussion." *Proc. 31st Biennial IAHR Congress*, Seoul, Korea, B.H. JUN, S.I. LEE, I.W. SEO and G.W. CHOI Editors, Theme E.4, Paper 0062, pp. 4037-4046 (ISBN 89 87898 24 5).
- KOCH, C., and CHANSON, H. (2006). "Unsteady Turbulence Characteristics in an Undular Bore." *Proc. Intl Conf. Fluvial Hydraulics River Flow 2006*, Lisbon, Portugal, 6-8 Sept., Topic A1, R.M.L. FERREIRA, E.C.T.L. ALVES, J.G.A.B. LEAL, and A.H. CARDOSO Eds., Balkema Publ., Taylor & Francis Group, London, Vol. 1, pp. 79-88 (ISBN 0 415 40815 6).

Numerical solution: $V_2 = -1.26$ m/s (flow reversal), $d_2 = 2.13$ m.

3. Application of the momentum principle to uniform equilibrium flow

3.1 In a rectangular concrete channel, the uniform equilibrium flow depth is 3.2 m. The channel is 2 m wide and the bed slope is 0.0006. Compute and give the values (and units) of the following quantities : (a) uniform equilibrium flow velocity, (b) Darcy friction factor, (c) discharge.

Solution: The problem is solved using the momentum principle. The bed shear stress must be estimated using the Darcy-Weisbach friction factor. See textbook pp. 69-77. Note that the calculations are iterative.

Numerical solution: $V_0 = 1.53 \text{ m/s}$, $d_0 = 3.2 \text{ m}$, $f = 0.0154$ ($k_s = 1 \text{ mm}$), $\tau_0 = 4.43 \text{ Pa}$

3.2. A rectangular channel (12-m wide) is faced with rubble masonry ($k_s = 50 \text{ mm}$). The total flow rate is $12.5 \text{ m}^3/\text{s}$ and the bed slope is 0.001.

(3.2.1) Compute and give the values and units of the following quantities : (a) uniform equilibrium flow depth, (b) Darcy friction factor, (c) boundary shear stress

(3.2.2) Is the uniform equilibrium flow sub- or super-critical ?

(3.2.3) From where would you control the flow ?

Numerical solution: $V_0 = 1.17 \text{ m/s}$, $d_0 = 0.891 \text{ m}$ (for $k_s = 50 \text{ mm}$)

3.3 A channel of trapezoidal cross-section (bottom width 2 m, sidewall slope 1V:3H) has a longitudinal slope of 0.012. The channel bed and sloping sidewall consist of a mixture of fine sands ($k_s = 0.2 \text{ mm}$). Uniform equilibrium flow conditions are achieved and the flow depth is 0.478-m.

(3.3.1) Compute and give the values and units of the following quantities : (a) flow rate, (b) uniform equilibrium flow velocity, (c) Darcy friction factor, (d) boundary shear stress, (e) shear Reynolds number, (f) critical flow depth.

(3.3.2) From where should the uniform equilibrium flow be controlled (upstream or downstream) ? Justify your answer.

Numerical solution: $V_0 = 4.82 \text{ m/s}$, $d_0 = 0.478 \text{ m}$, $\tau_0 = 38.4 \text{ Pa}$, $d_c = 0.80 \text{ m}$

3.4. A channel of rectangular cross-section (bottom width 15 m) has a longitudinal slope of 0.002. The channel bed and sloping sidewall consist of a bush ($n_{\text{Manning}} = 0.05 \text{ s/m}^{1/3}$). Uniform equilibrium flow conditions are achieved and the total flow rate equals $21 \text{ m}^3/\text{s}$. Compute and give the values (and units) of the following quantities : (a) uniform equilibrium flow depth (i.e normal depth), (b) uniform equilibrium flow velocity, (c) critical flow depth.

Numerical solution: $V_0 = 1.0 \text{ m/s}$, $d_0 = 1.4 \text{ m}$

3.5 Flood plain calculations

Considering the flood plain, sketched in figure E.4.2 (textbook, p. 92), the mean channel slope is 0.05 degrees. The river channel is lined with concrete and the flood plain is riprap material (equivalent roughness height : 8 cm). The fluid is water with a heavy load of suspended sediment (fluid density : $1,080 \text{ kg/m}^3$). The flow is assumed uniform equilibrium. Compute and give the values and units of the following quantities :

(a) Volume discharge in the river channel. (b) Volume discharge in the flood plain. (c) Total volume discharge (river channel + flood plain). (d) Total mass flow rate (river channel + flood plain). (e) Is the flow subcritical or supercritical ? Justify your answer clearly.

Assume no friction (and energy loss) at the interface between the river channel flow and the flood plain flow.

Numerical solution: $V_0 = 3.44 \text{ m/s}$ (river), $V_0 = 1.62 \text{ m}$ (flood plain), $Q = 154 \text{ m}^3/\text{s}$ (river), $Q = 350 \text{ m}^3/\text{s}$ (flood plain)

More exercises in textbook pp. 46-49, 87-93, 111-118.

"The Hydraulics of Open Channel Flow: An Introduction", *Butterworth-Heinemann Publ.*, Oxford, UK, 2004.

More Exercises at : {<http://www.bh.com/companions/0340740671/>}

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